

Electromigration-aware Interconnect Design

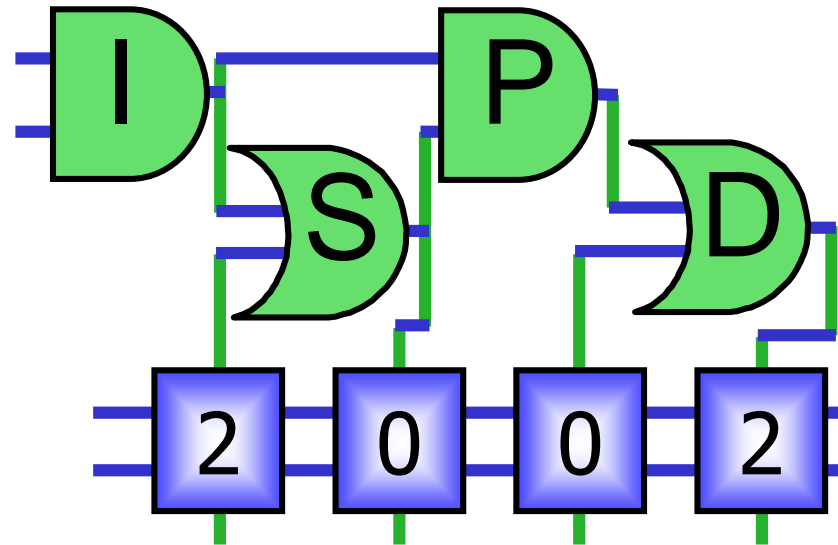
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Acknowledgments

Vivek Mishra (PhD 16), Palkesh Jain (PhD 17)
Vidya Chhabria (PhD student)





International Symposium on Physical Design
 San Diego, CA April 9-12, 2000



International Symposium on Physical Design

April 14 - 17, 2019
 San Francisco, California, USA

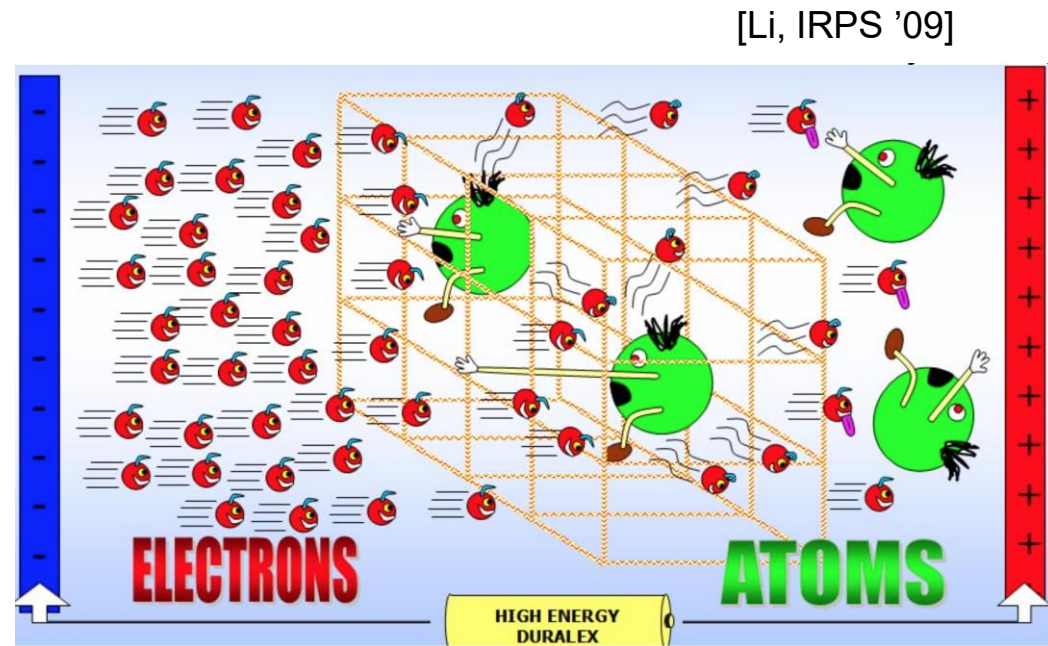
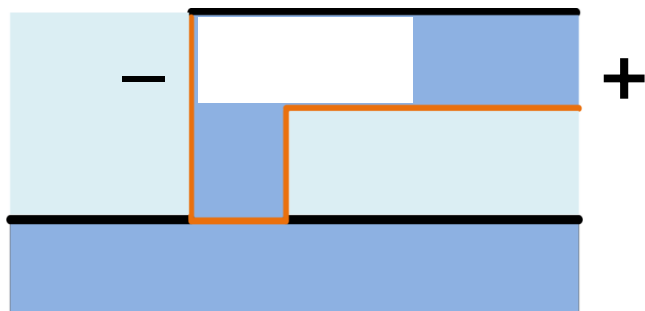
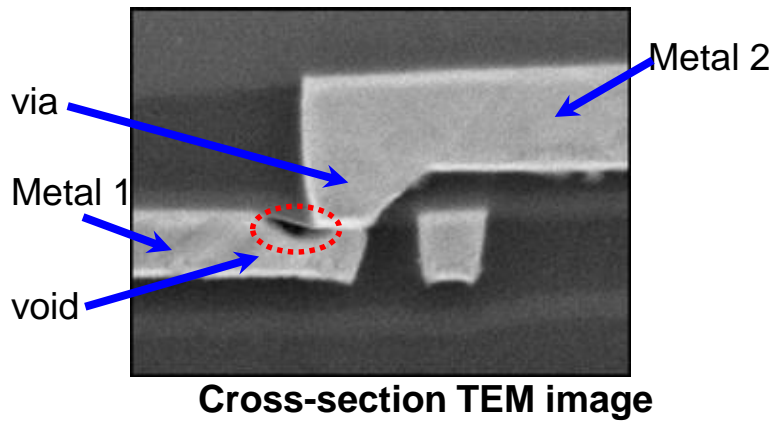



Outline

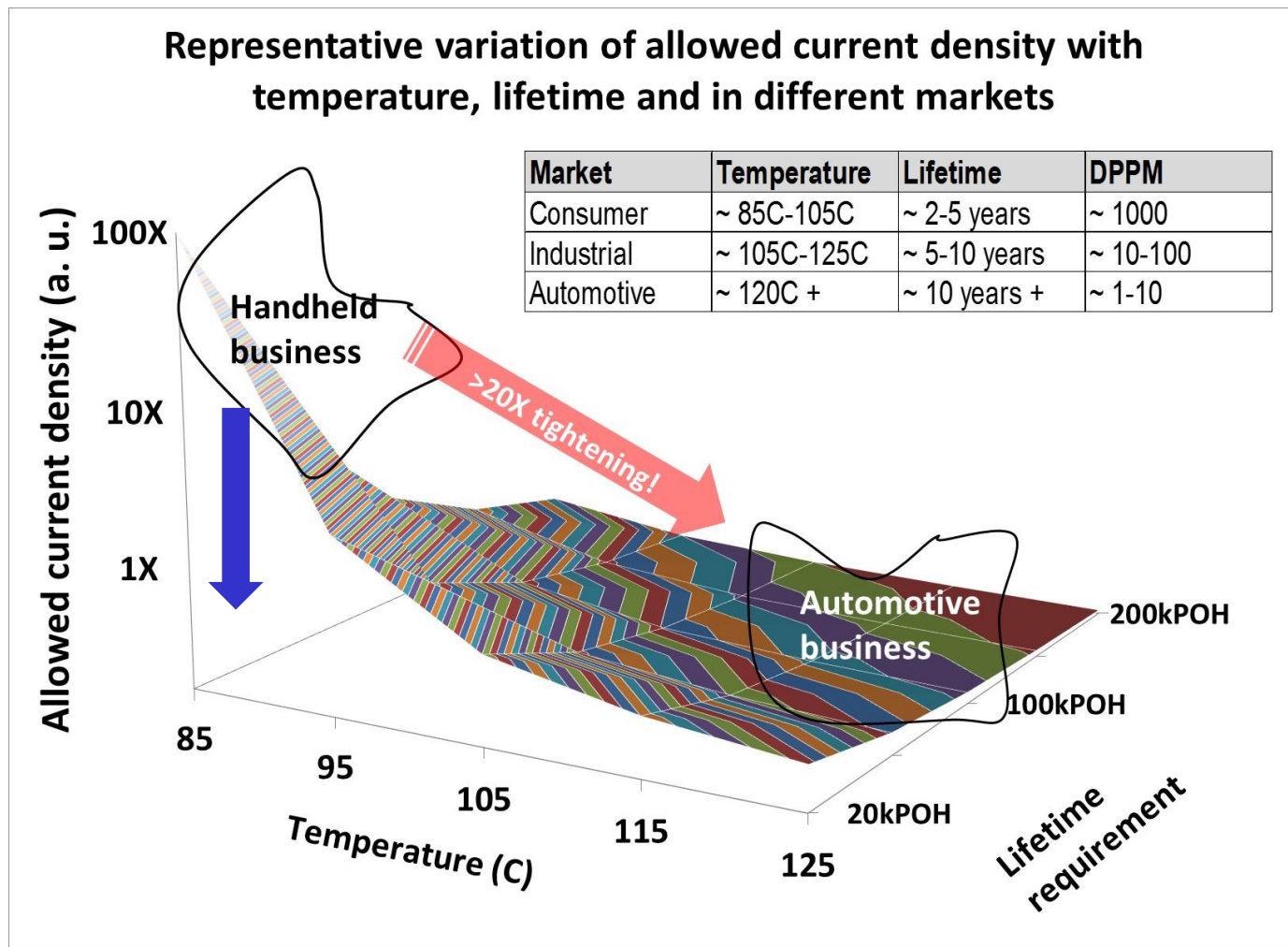
- Overview of electromigration
- EM modeling
- The weakest-link model (and why it's problematic)

Interconnect aging

- Electromigration (EM)



Traditional view of EM



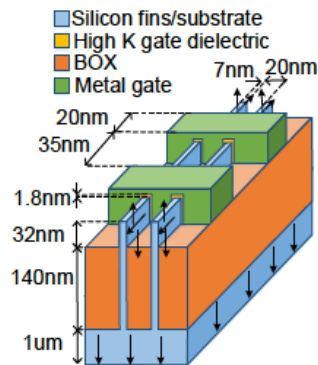
+ I/O drivers

+ FinFETs, GAAFETs

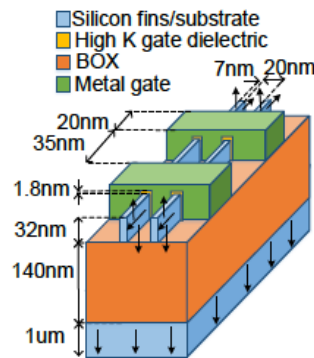
[Jain, TVLSI June 16]

Self heating

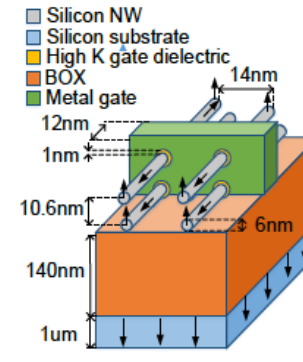
- Joule heating in wires
- Multigate FETs make things worse
 - Larger degrees of self-heating, worse paths to the ambient



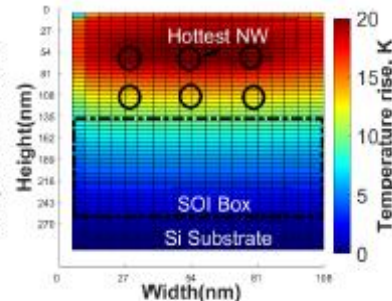
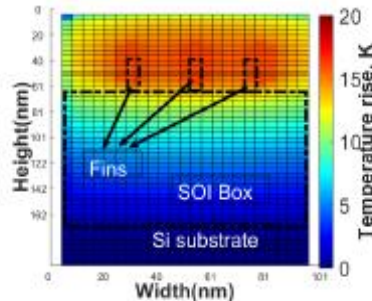
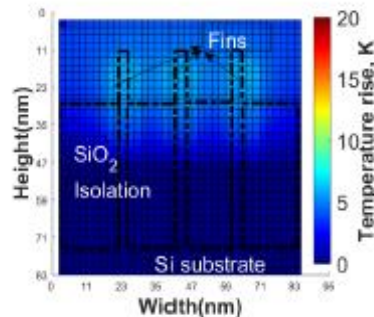
Bulk FinFET



SOI FinFET



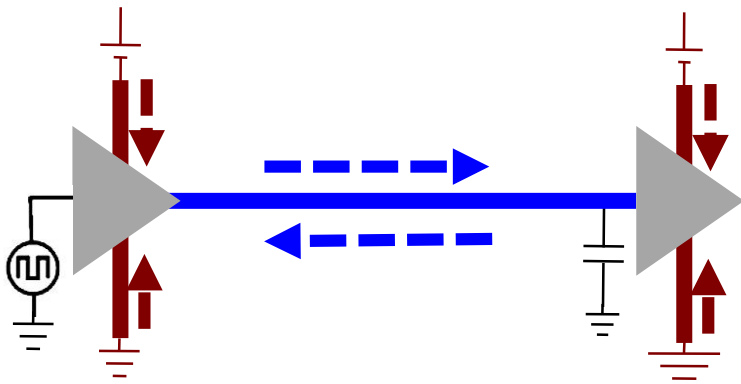
GAAFET



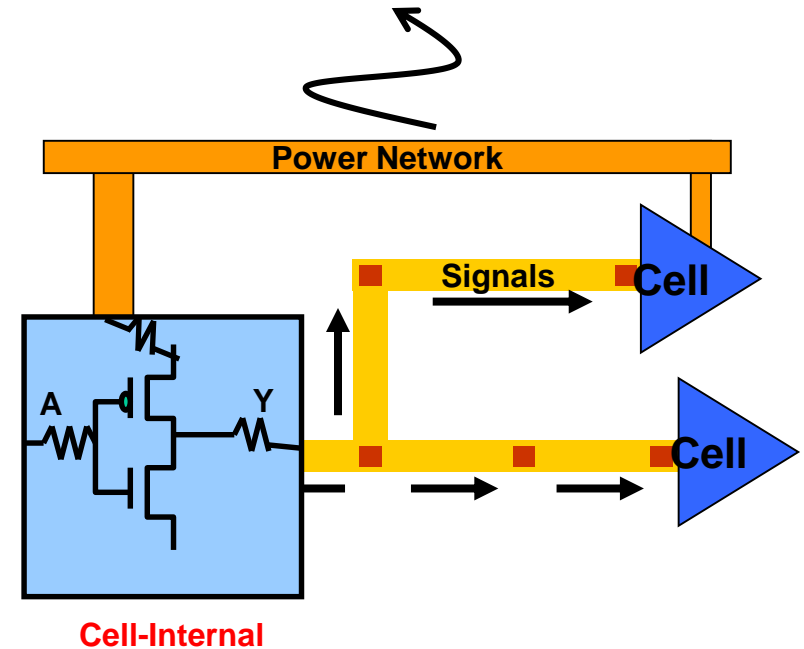
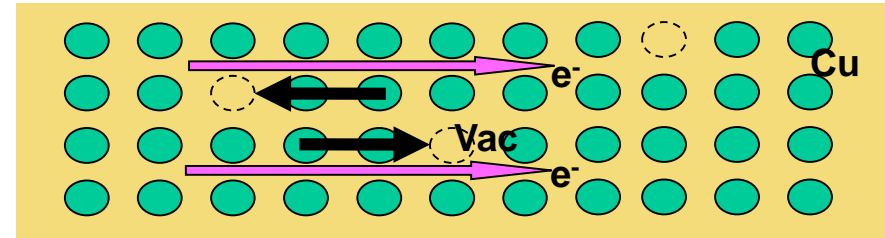
[Chhabria, ISQED 19]

Which interconnects?

- Power grids
 - Largely unidirectional current
- Signal interconnects
 - Bidirectional current flow
 - Recovery effects seen



■ DC
■ AC



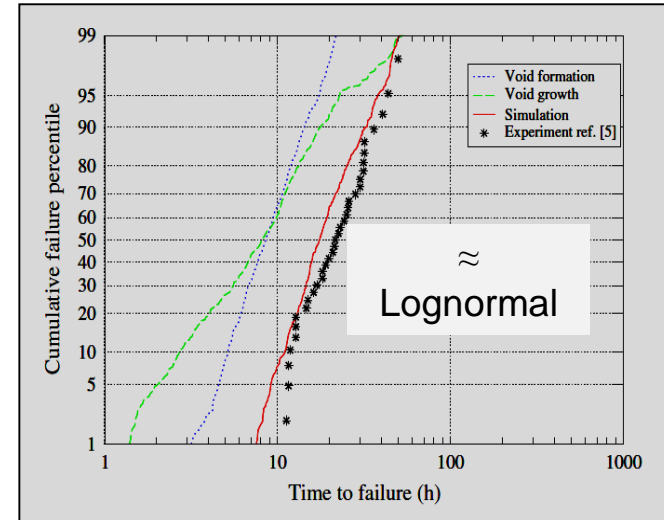
Outline

- Overview of electromigration
- EM modeling
- The weakest-link model (and why it's problematic)

Black's law

- Black's law
 - Predicts mean time to failure

$$t_{50} = A j_{AVG}^{-n} \exp\left(\frac{Q_{EM}}{k_B T}\right); \Delta T \propto j_{RMS}^2$$



- TTF follows a lognormal distribution

- For a fail fraction FF , defects in parts per million (DPPM)

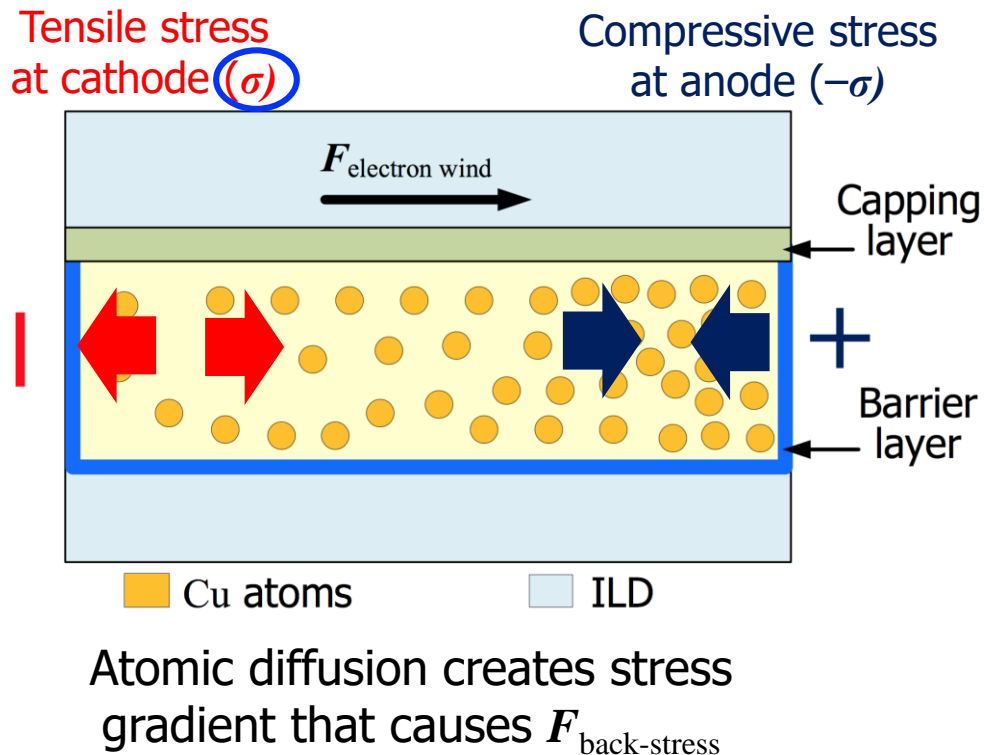
$$t_z = t_{50} e^{z/\sigma} \qquad FF = \int_{-\infty}^z \frac{e^{-x^2/2}}{\sqrt{2\pi}} dx$$

- Constraint on $t_z \rightarrow$ Constraint on $t_{50} \rightarrow$ Constraint on j_{AVG}
- Joule heating \rightarrow Constraint on j_{RMS}

- Circuit-level EM constraint:

- For **each wire**, stay within $j_{RMS,max}$, $j_{AVG,max}$

Physics of mortality and the Blech criterion



Blech criterion

At steady state,
 $F_{\text{electron wind}} = F_{\text{back-stress}}$

If: At steady state, $\sigma < \sigma_{\text{critical}}$
then: wire is immortal!
 (voids never form)

$\sigma < \sigma_{\text{critical}} \Rightarrow J \times L < K_1$ (Blech criterion)

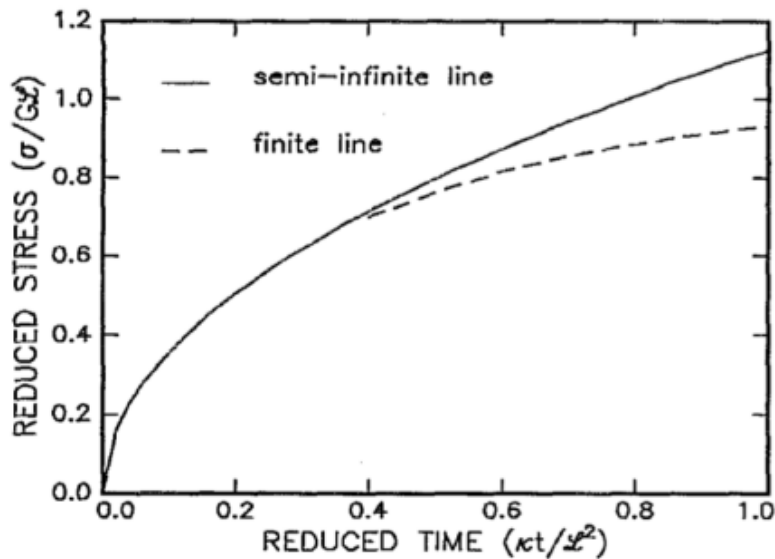
σ_{critical} : Critical stress needed for void formation

Physics-based EM analysis

- Korhonen model
 - Void nucleation

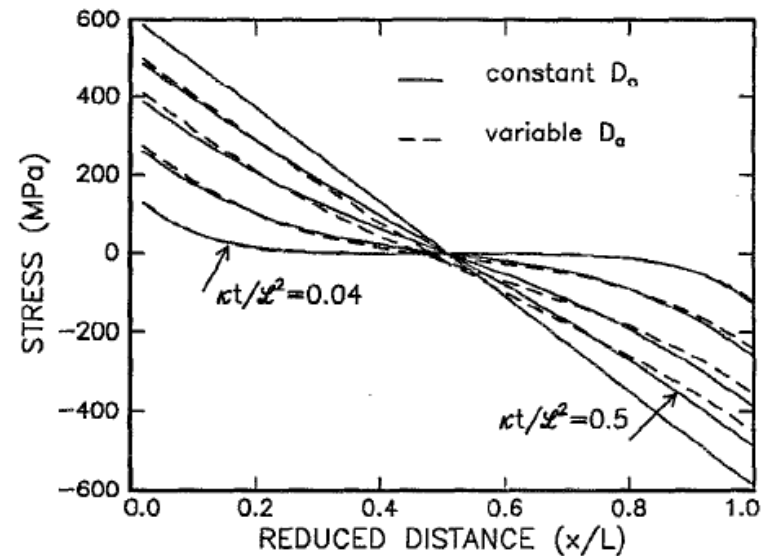
$$\frac{\partial \sigma_H}{\partial t} = \frac{\partial}{\partial x} \left[\kappa \left(\frac{\partial \sigma_H}{\partial x} + G \right) \right]$$

$$\frac{\partial \sigma}{\partial t} = \frac{\partial}{\partial x} \left[\kappa (F_{\text{back-stress}} + F_{\text{electron wind}}) \right]$$



Stress at a blocking boundary (cathode)

[Korhonen, JAP 1993]



Stress evolution along the wire

EM mortality: Issues with classical approach

Blech criterion

if: $J \times L < K_1$
Wire immortal to EM
else: wire is
potentially mortal

**Steady state
approach** for
mortality

Black's equation

For potential
mortal wires:

$$\text{TTF} = \frac{K_2}{J^n} \exp\left(\frac{K_3}{T}\right)$$

Empirical model,
issues for Cu

[Lloyd, MER '07]

EM mortality: Classical vs. filtering approach

Blech criterion

if: $J \times L < K_1$
Wire immortal to EM
else: wire is
potentially mortal

**Steady state
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Black's equation

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Empirical model,
issues for Cu

[Lloyd, MR '07]

Filtering approach

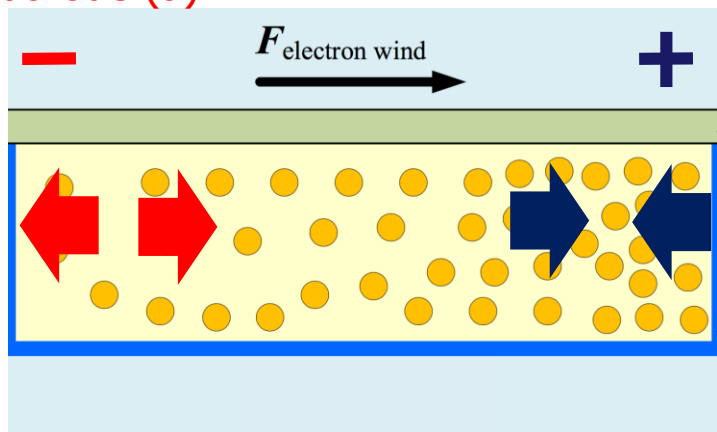
**Transient
state** approach
for mortality

Physics-based,
applicable for Cu

EM mortality: Mechanical stress evolution

Tensile stress at cathode (σ)

Compressive stress at anode ($-\sigma$)

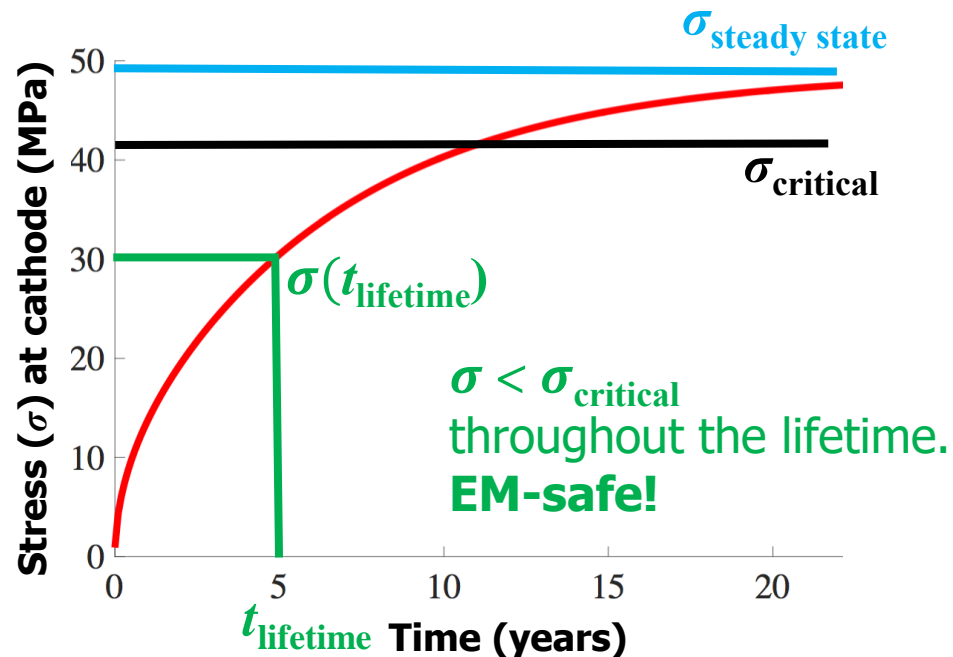


○ Cu atoms

Atomic diffusion creates stress gradient that causes $F_{\text{back-stress}}$

Blech criterion presumes **steady state** between $F_{\text{electron wind}}$ and $F_{\text{back-stress}}$

Potentially mortal by Blech criterion



1. **Practical EM mortality: relative to the product lifetime**
2. **Transient stress evolution instead of steady state**

EM mortality: Modeling transient stress

EM equation

$$\frac{\partial \sigma}{\partial t} = \frac{\partial}{\partial x} [\kappa (F_{\text{back-stress}} + F_{\text{electron wind}})]$$

Stress at cathode, $\sigma(t)$, 2 options:

1. **Semi-infinite (SI):**

$$\sigma(t) = \alpha_1 J \sqrt{t}$$

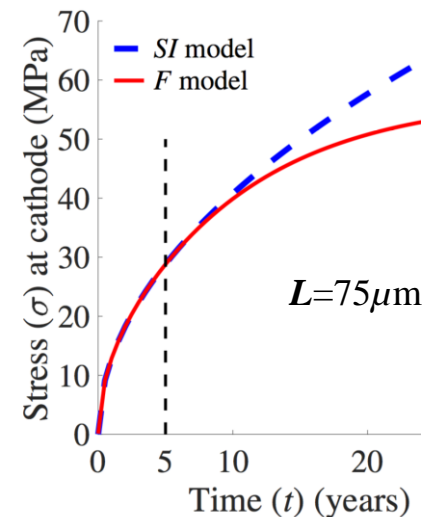
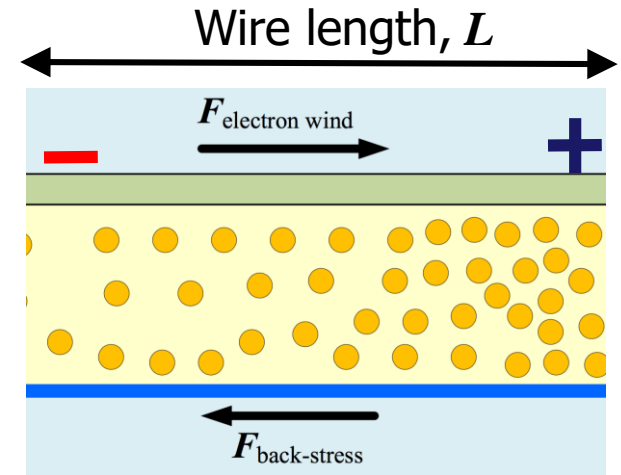
Efficient, but overestimates stress

2. **Finite (F):**

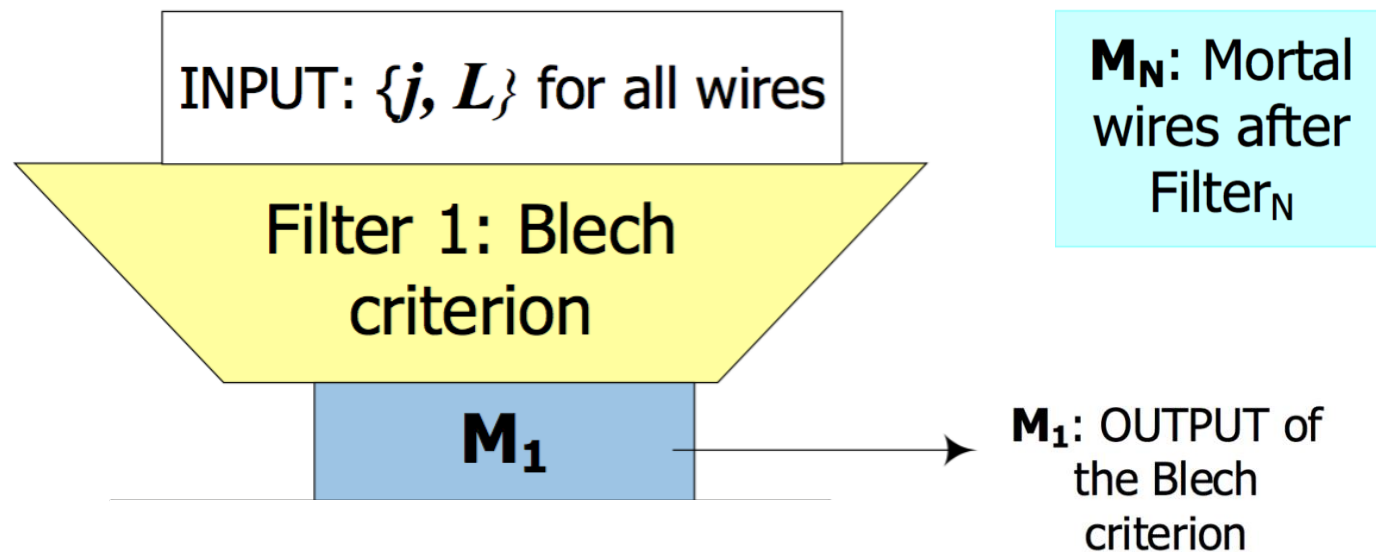
$$\sigma(t) = J L \alpha_2 \left(\frac{1}{2} - \sum_{n=0}^{\infty} \frac{e^{-m_n^2 \frac{t \alpha_2}{L^2}}}{m_n^2} \right)$$

Inefficient, but accurate prediction

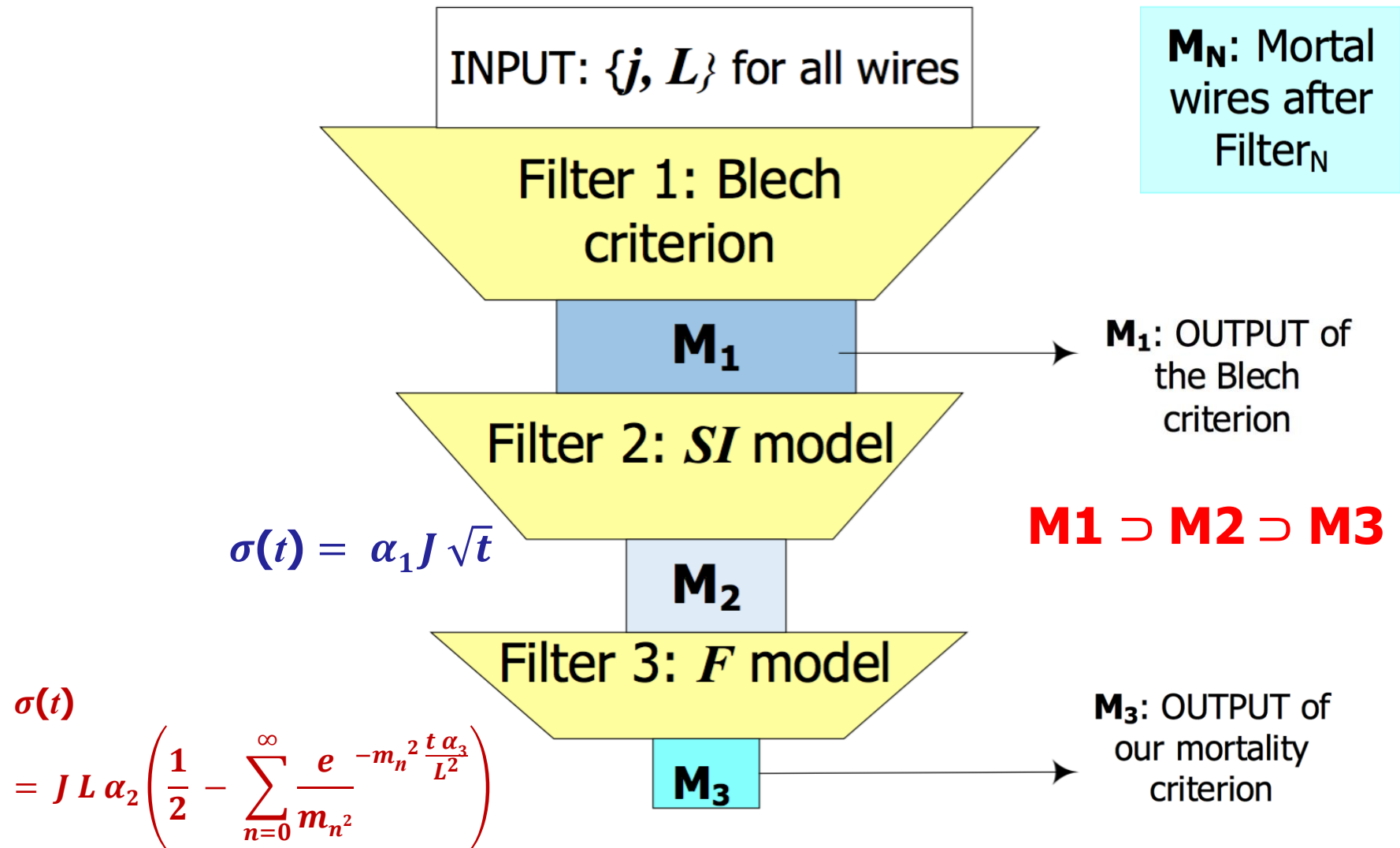
Extension to interconnect trees using [Park, IRPS10]



Sequential mortal wire filtration

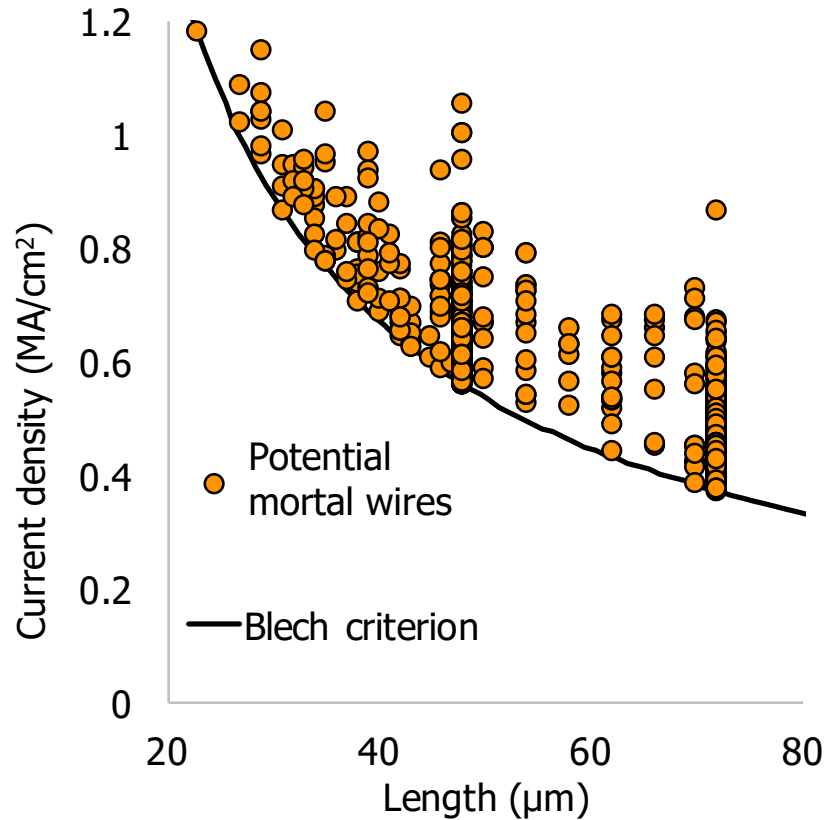


Sequential mortal wire filtration



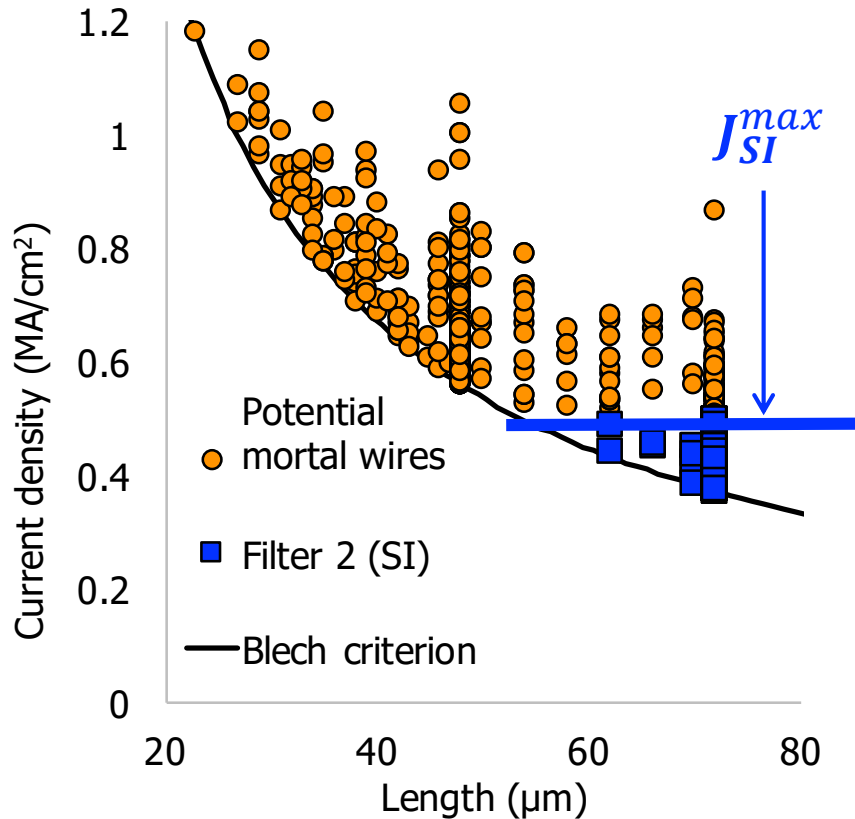
IBMPG case study: PG2 mortal wire distribution

Potential Mortal wires from the Blech criterion



IBMPG case study: PG2 mortal wire distribution

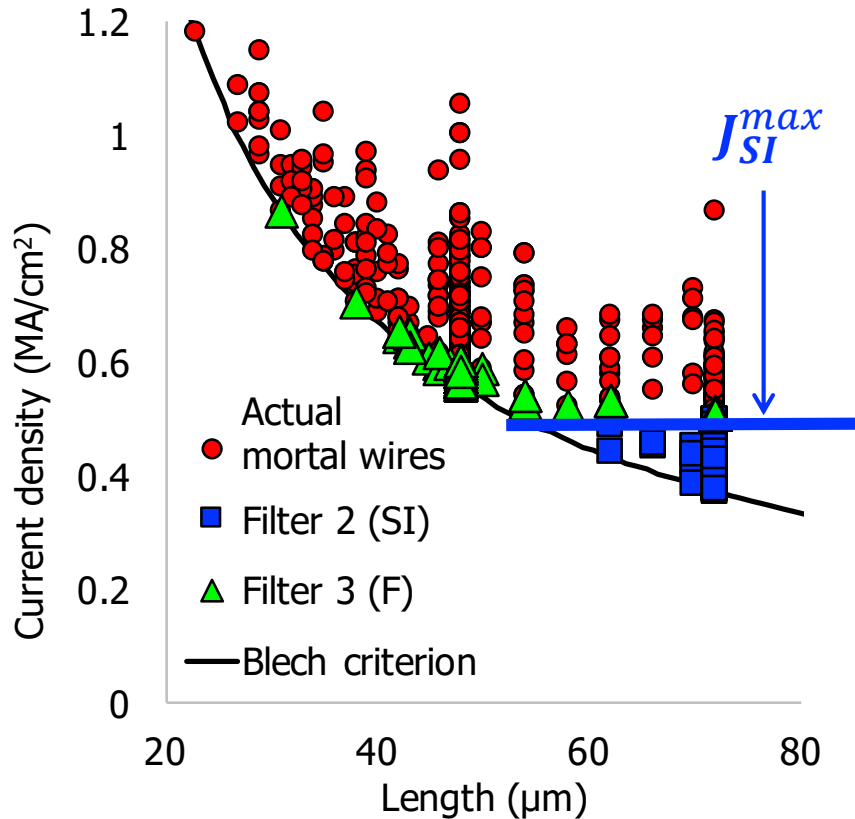
Immortal wires filtered out using pessimistic Filter 2 (SI)



Product lifetime = 10 years
Temperature (T) = 105C

IBMPG case study: PG2 mortal wire distribution

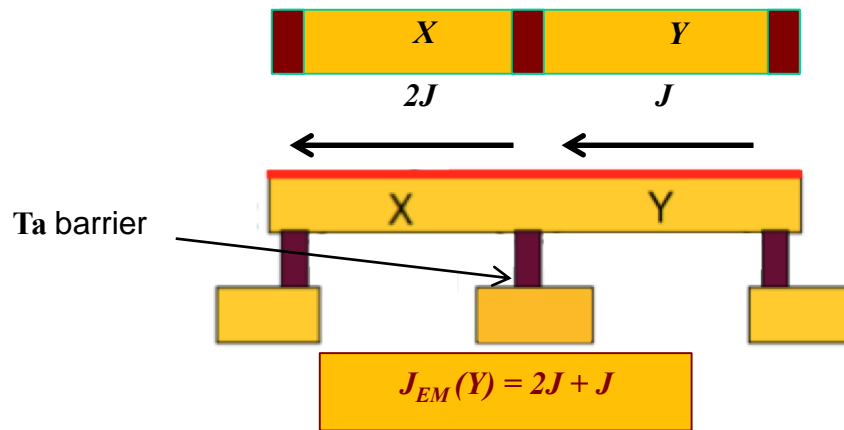
Immortal wires filtered out using pessimistic Filter 2 (SI) & accurate Filter 3 (F)



Product lifetime = 10 years
Temperature (T) = 105C

What about lines with branches? Vias?

- Flux Divergence
 - Current flow in neighboring wire affects EM flux
 - Use effective current for EM



- The above is approximate
 - There's a physics-based version for this too

[Park, IRPS10]

Outline

- Overview of electromigration
- EM modeling
- The weakest-link model (and why it's problematic)

Circuit impact

- Conventional way to overcome EM

$$t_z = t_{50} e^{z/\sigma} \quad t_{50} = A j_{AVG}^{-n} \exp\left(\frac{Q_{EM}}{k_B T}\right)$$

- Constraint on $t_z \rightarrow$ Constraint on $t_{50} \rightarrow$ Constraint on j_{AVG}
 - Joule heating \rightarrow Constraint on j_{RMS}
- Circuit-level EM constraint:
 - For **each wire**, stay within $j_{RMS,max}$, $j_{AVG,max}$
 - Weakest-link model



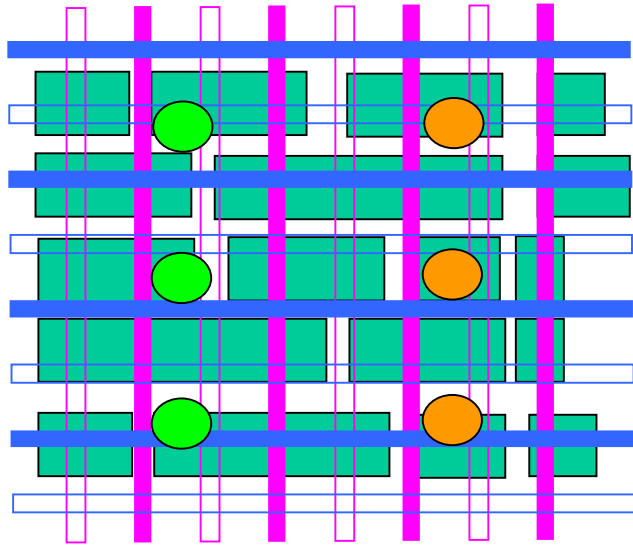
Handling catastrophic errors



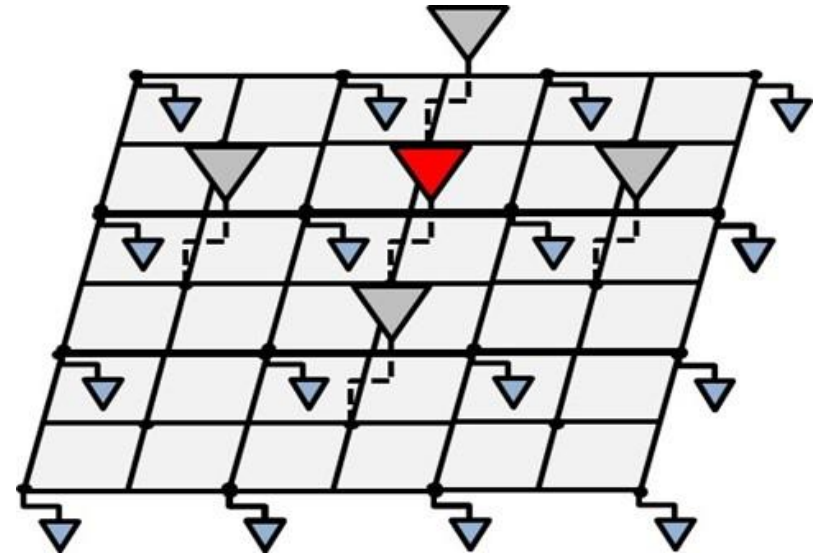
- A simple analysis of an n -component system
 - F_i = probability of failure of the i^{th} component
 - $1 - F_i$ = probability that the i^{th} component works
 - n = number of components in the system
 - $(1 - F_i)^n$ = probability that all n components work
 - Probability of system failure = $1 - (1 - F_i)^n$
- Implicit assumptions
 - All failures are catastrophic
 - All failures are equally serious
 - All failures are independent

Interconnect redundancy

- Several on-chip interconnect systems are built to be redundant



Power grids

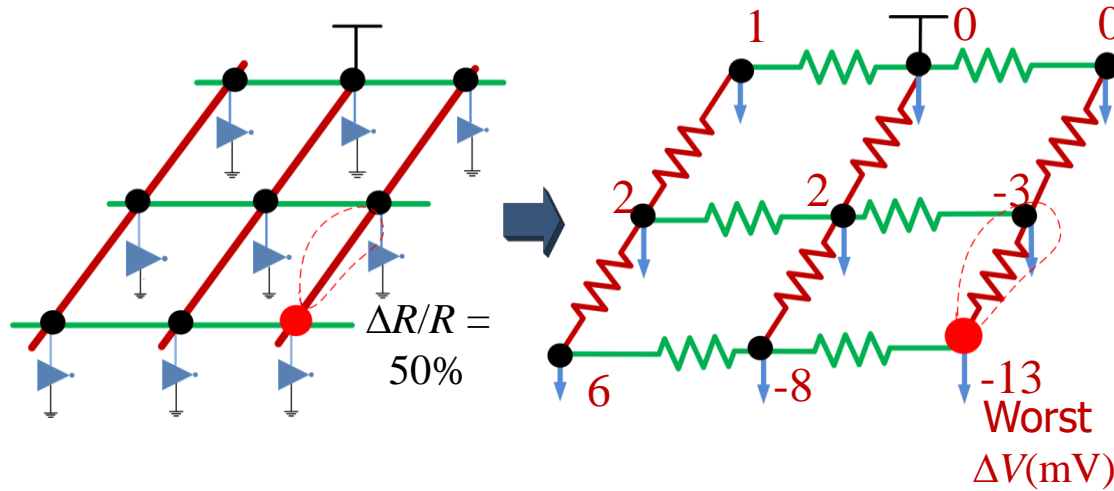


Clock grids

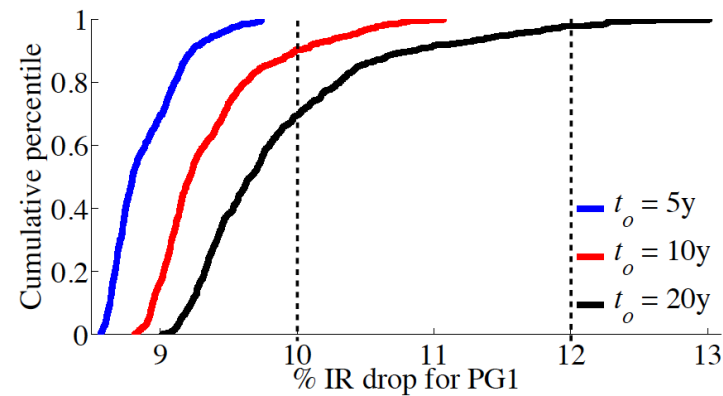
- A system fails when it's key parameters fail – and NOT at first failure!

Electromigration in power grids

- Power grids are built to contain redundancies!

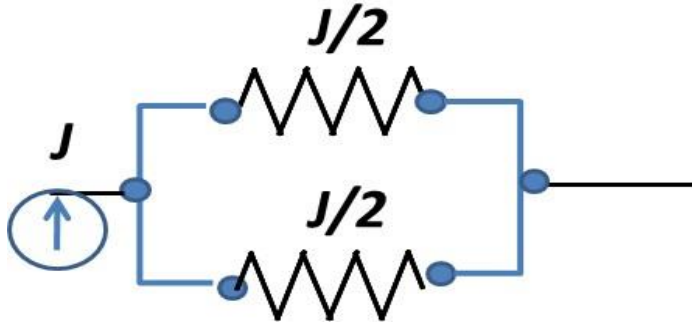


A better failure criterion:

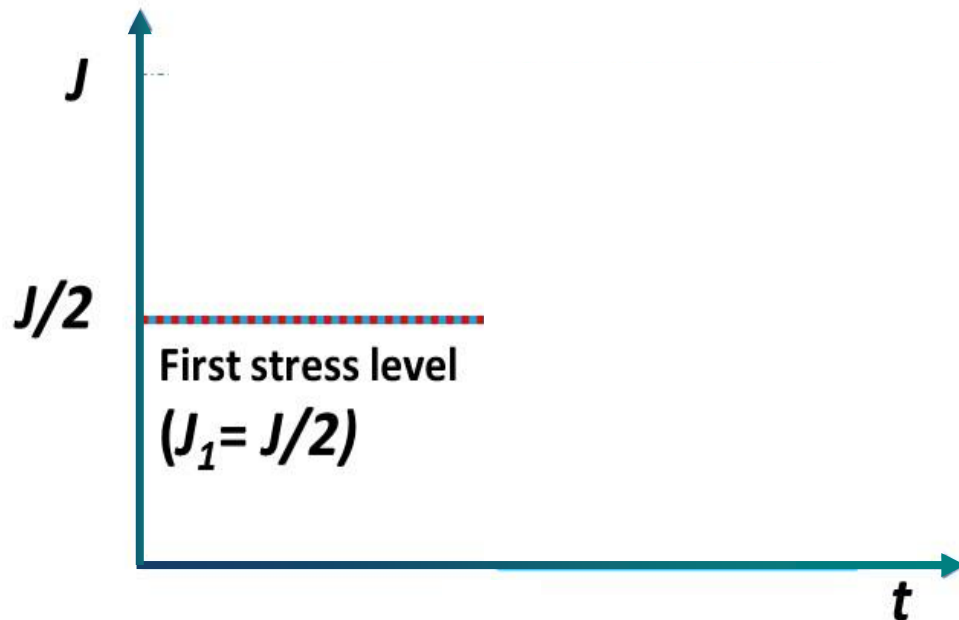


[Mishra, DAC13]

Analyzing redundancy

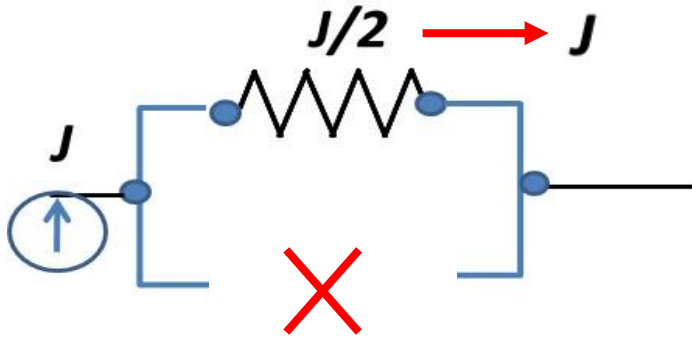


- Two component system: one of the two fails first



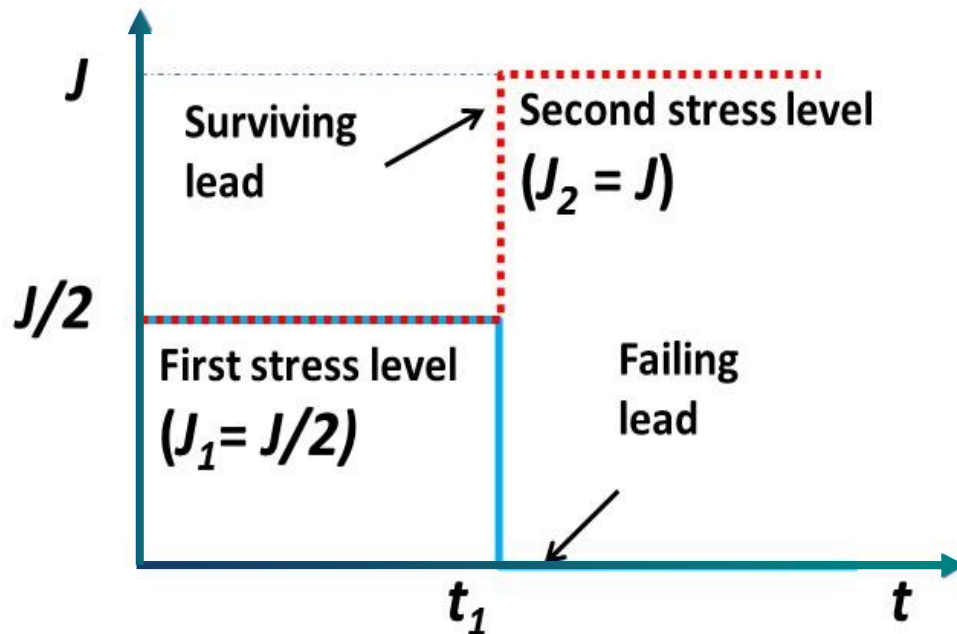
[Jain, IRPS15]

Analyzing redundancy



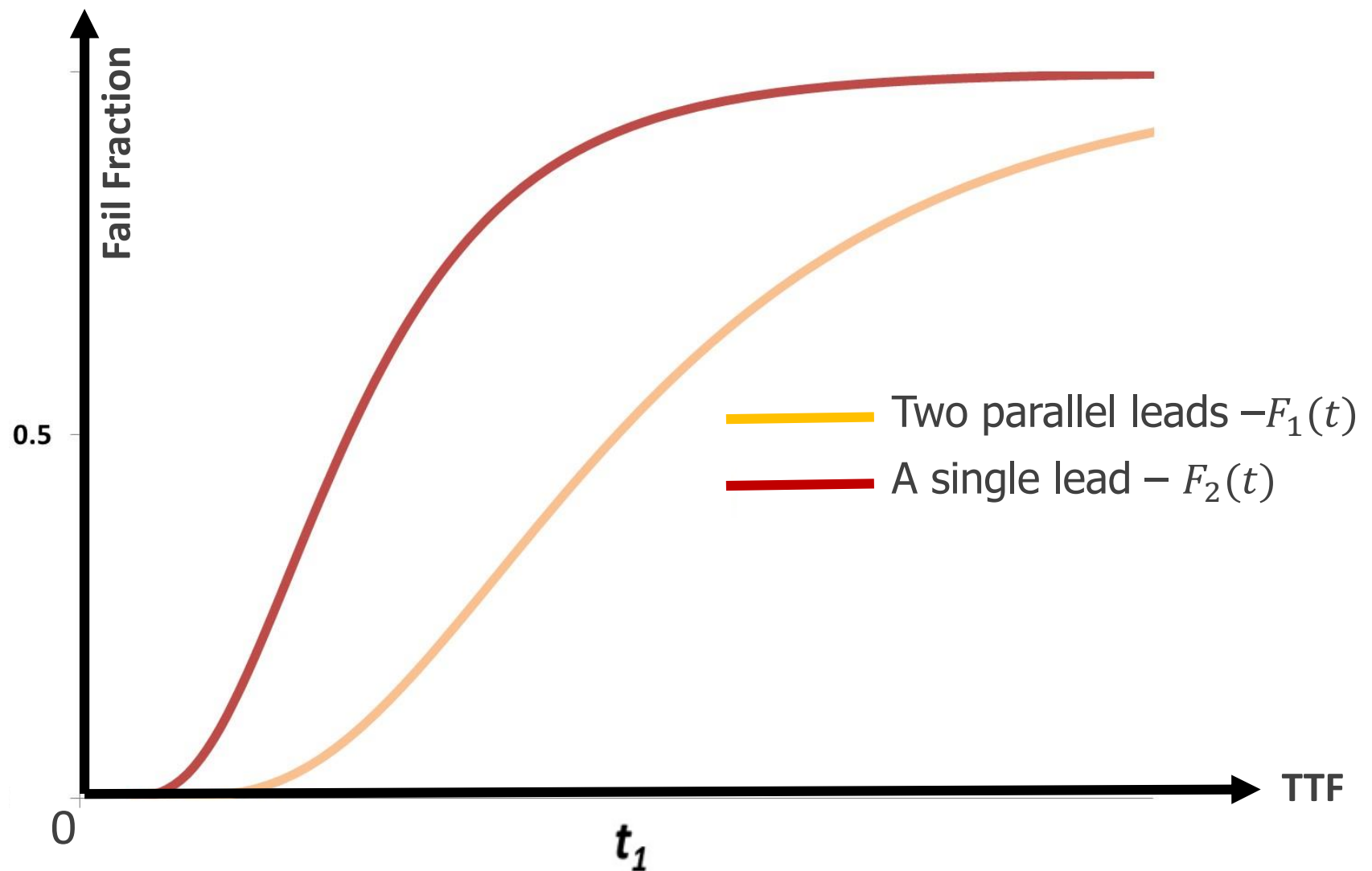
- Two-component system: one of the two fails first

- Post-failure: current goes through intact component



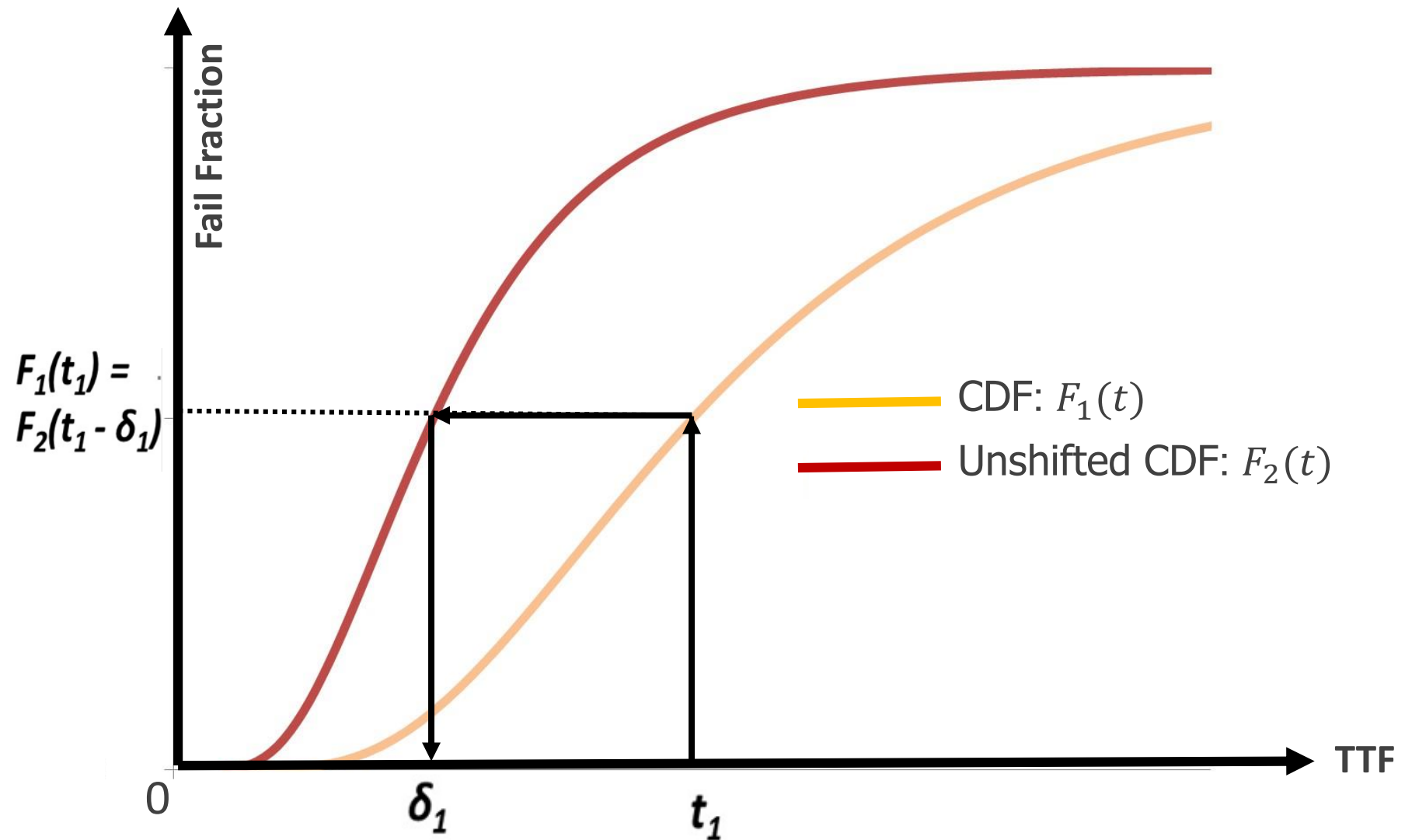
[Jain, IRPS15]

Reliability under changing stress



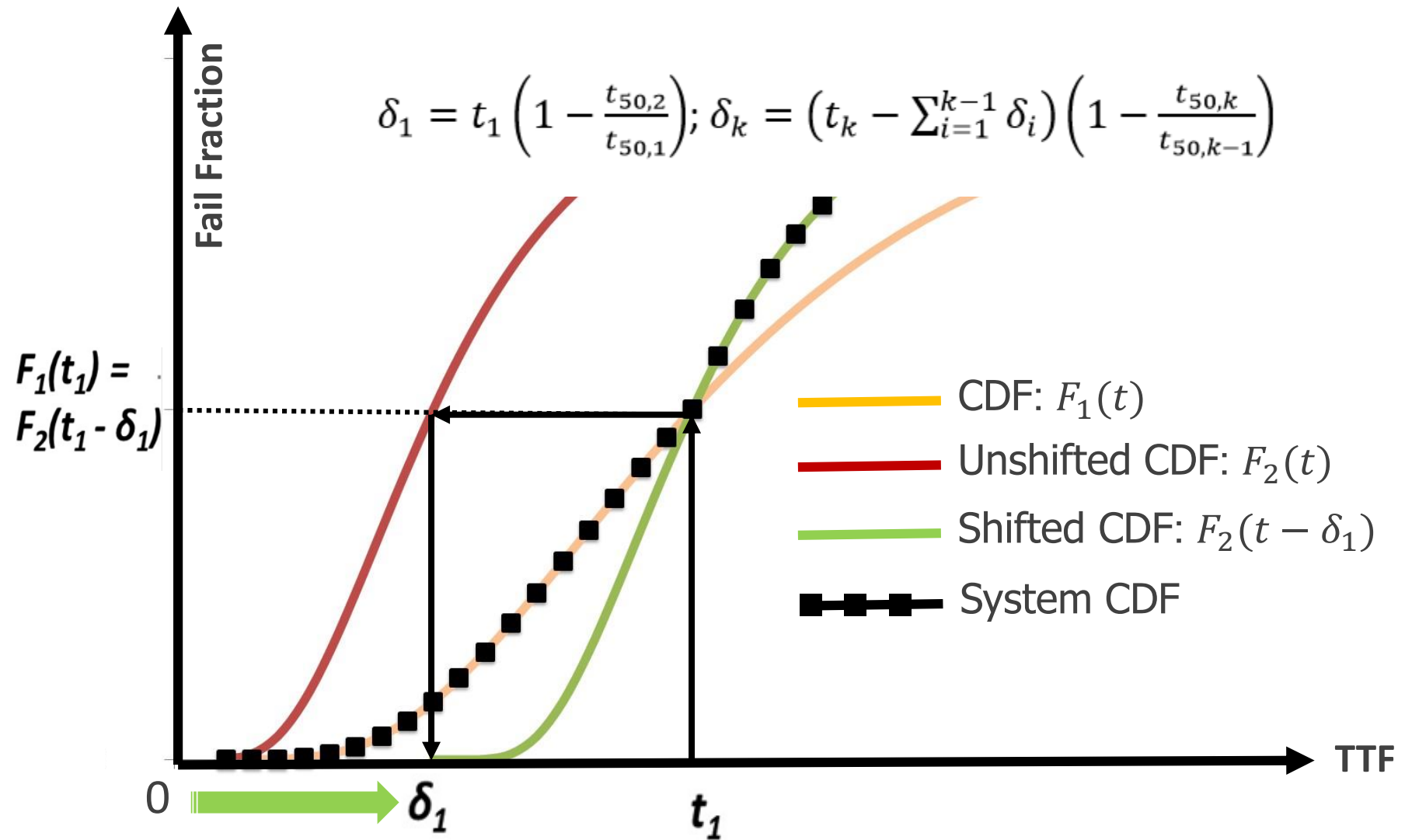
[Jain, IRPS15]

Reliability under changing stress



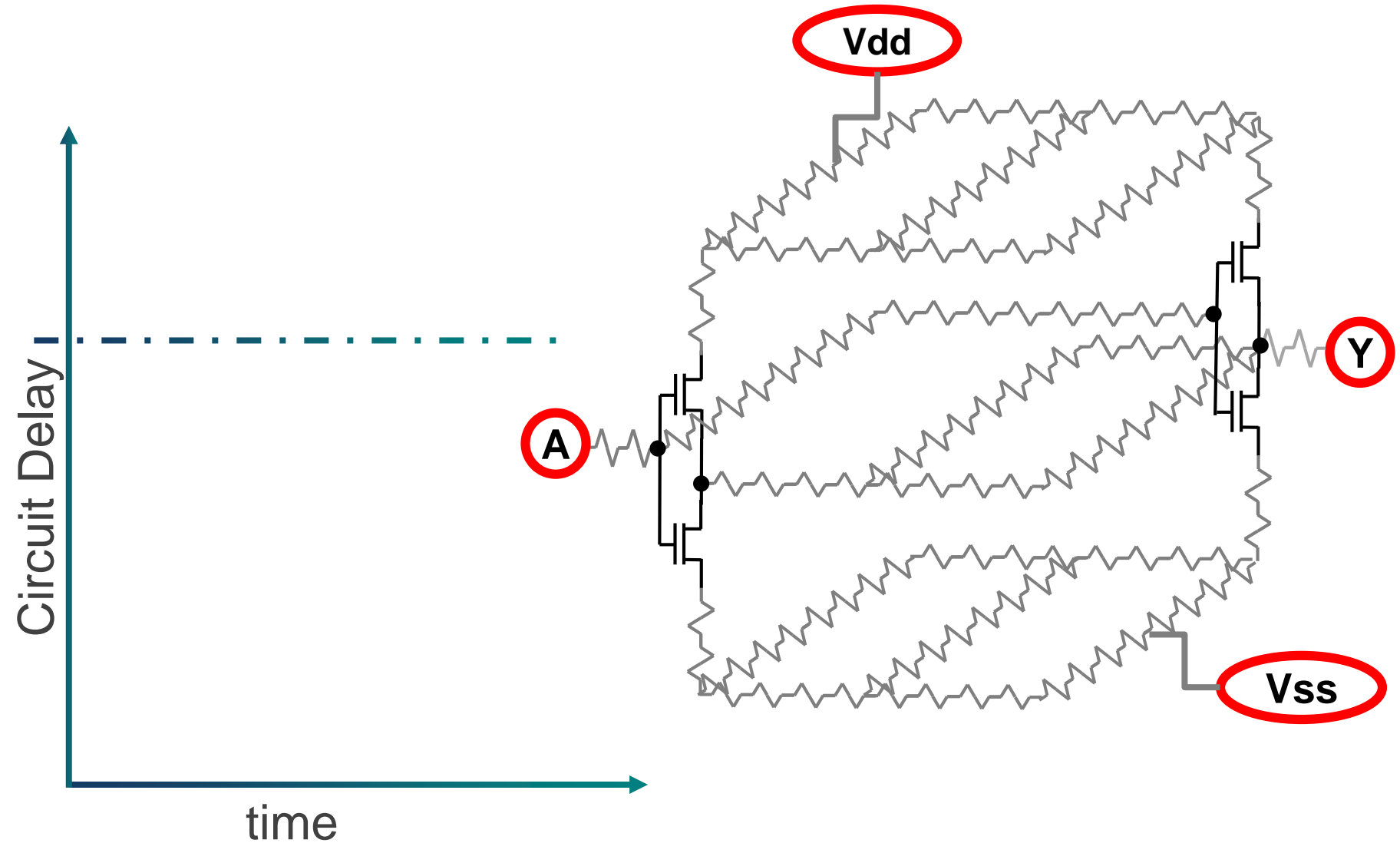
[Jain, IRPS15]

Reliability under changing stress



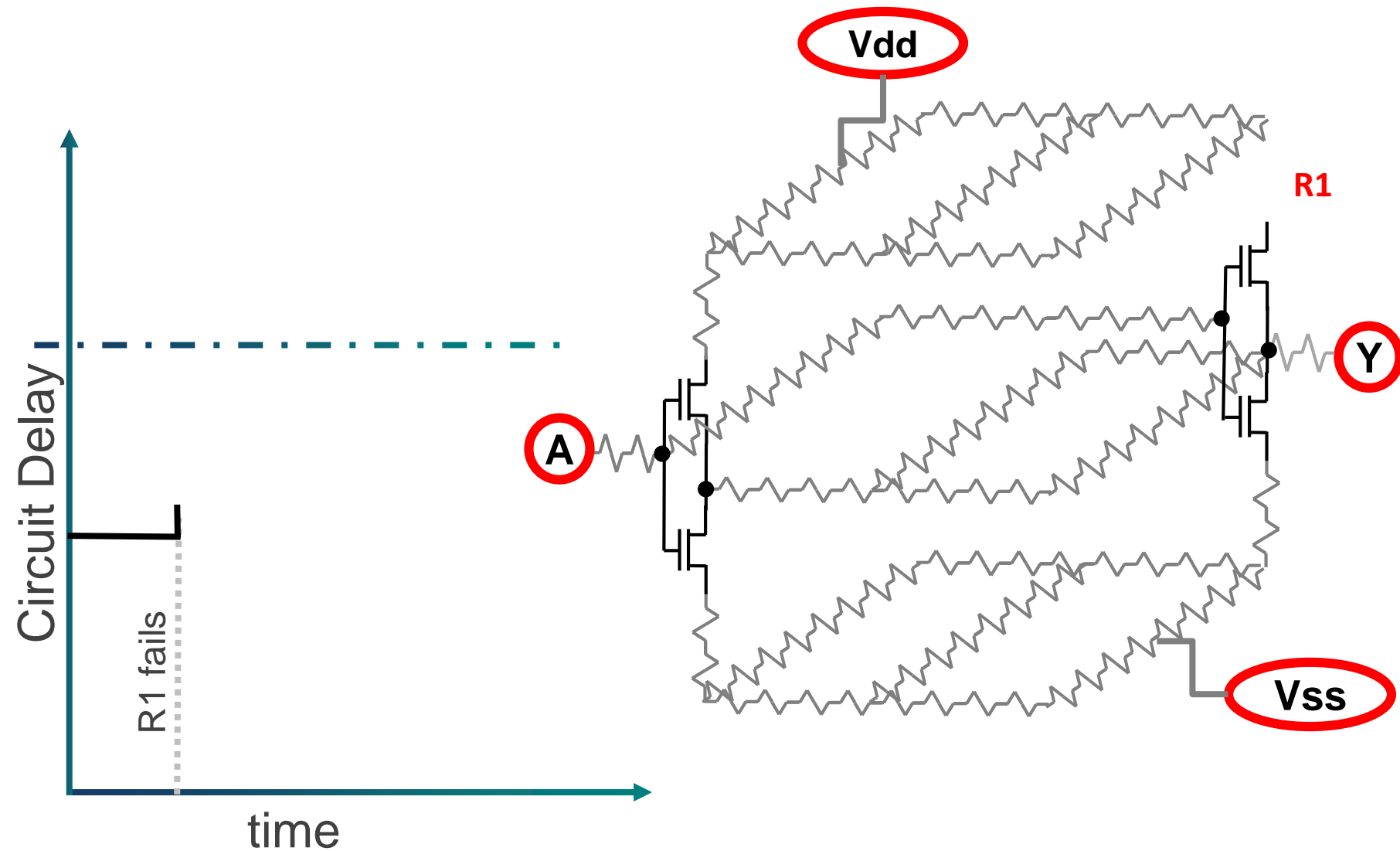
[Jain, IRPS15]

System impact for a clock grid



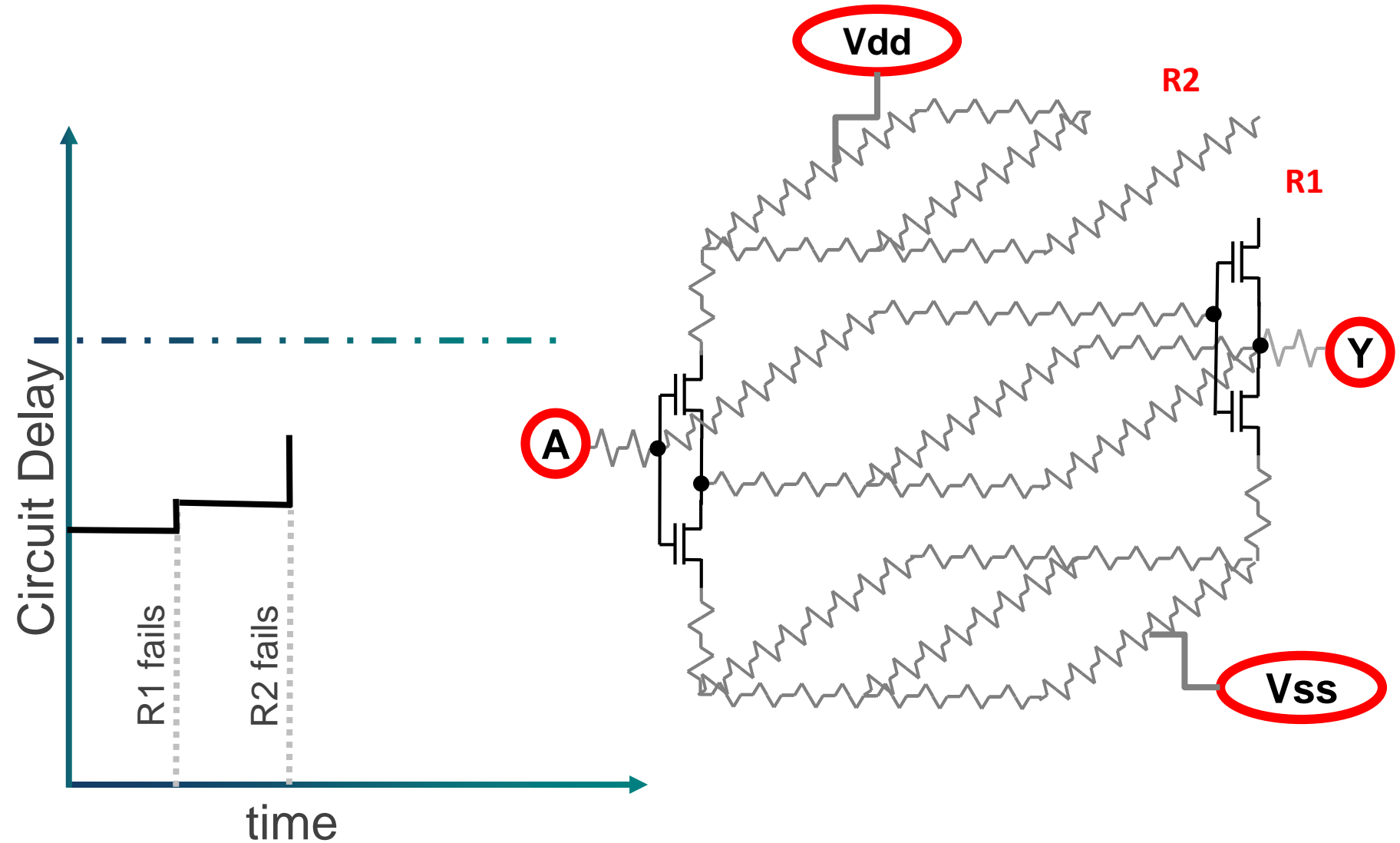
[Jain, IRPS15]

System impact for a clock grid



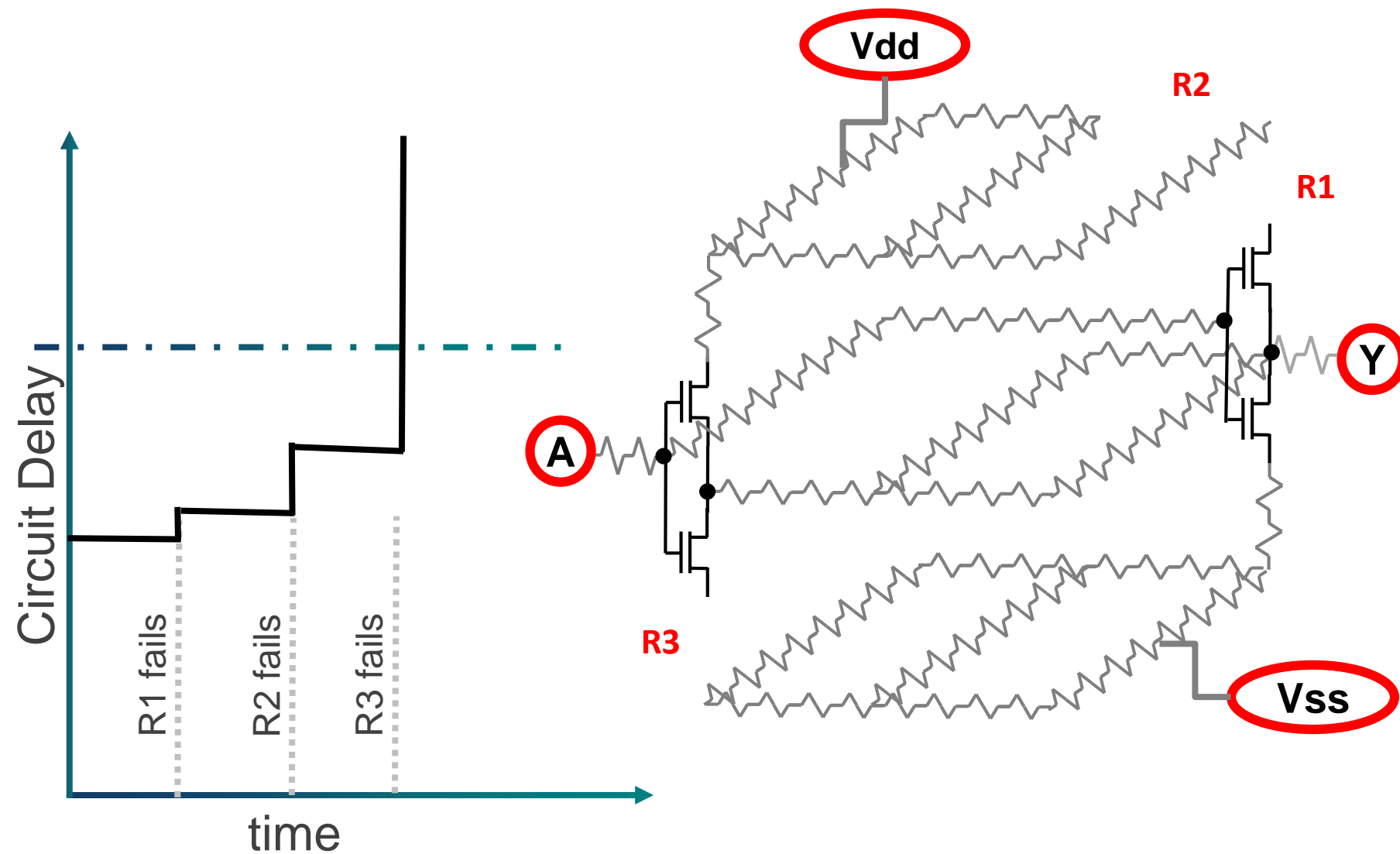
[Jain, IRPS15]

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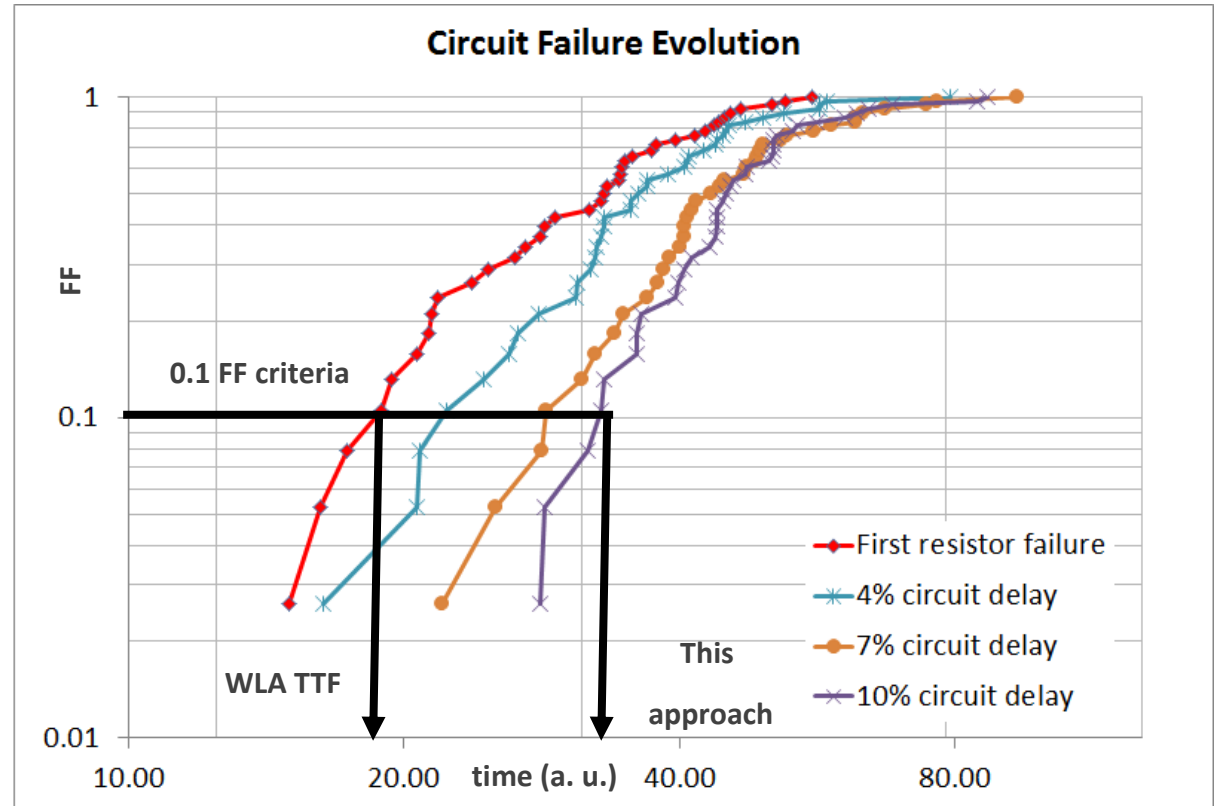
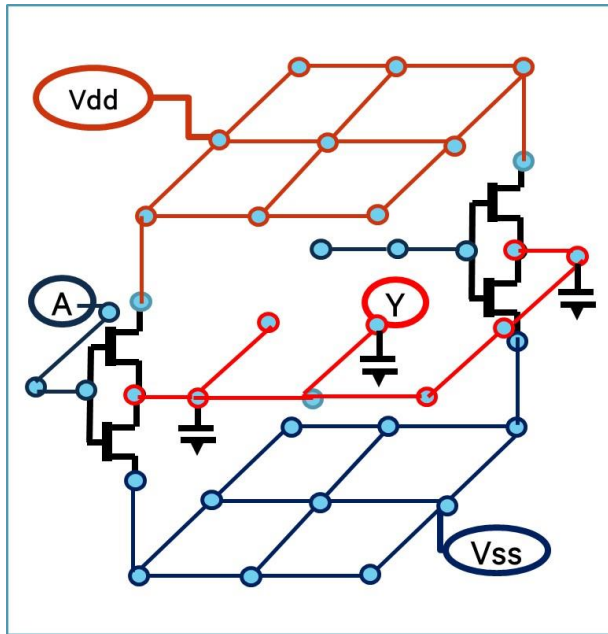
[Jain, IRPS15]

System impact for a clock grid



[Jain, IRPS15]

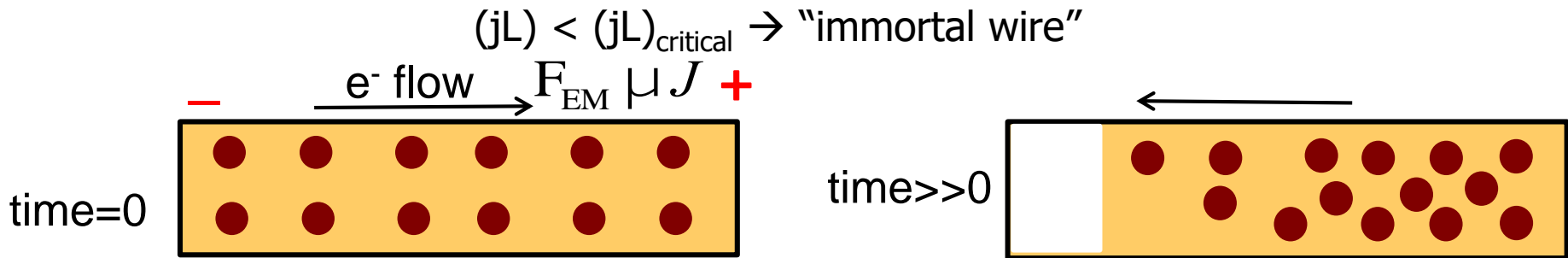
Quantitative evaluation



[Jain, IRPS15]

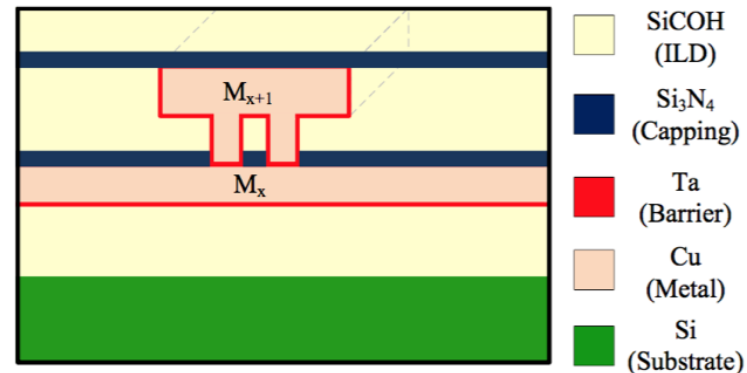
EM and stress

- Blech effect
 - Back stress opposes electron wind
 - Some wires are “immortal” due to back-stress



- Other sources of stress – thermomechanical stress

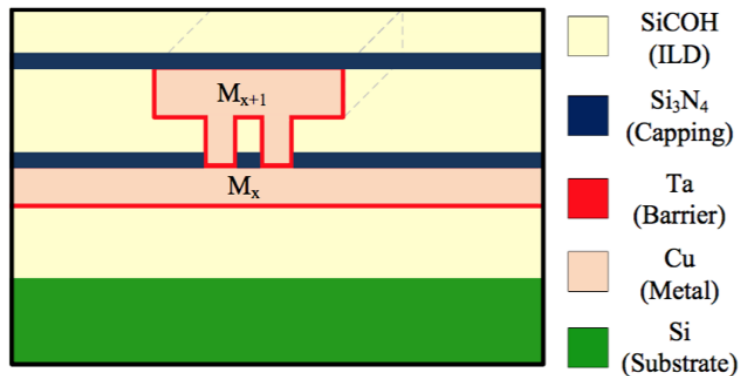
Typical Cu interconnect



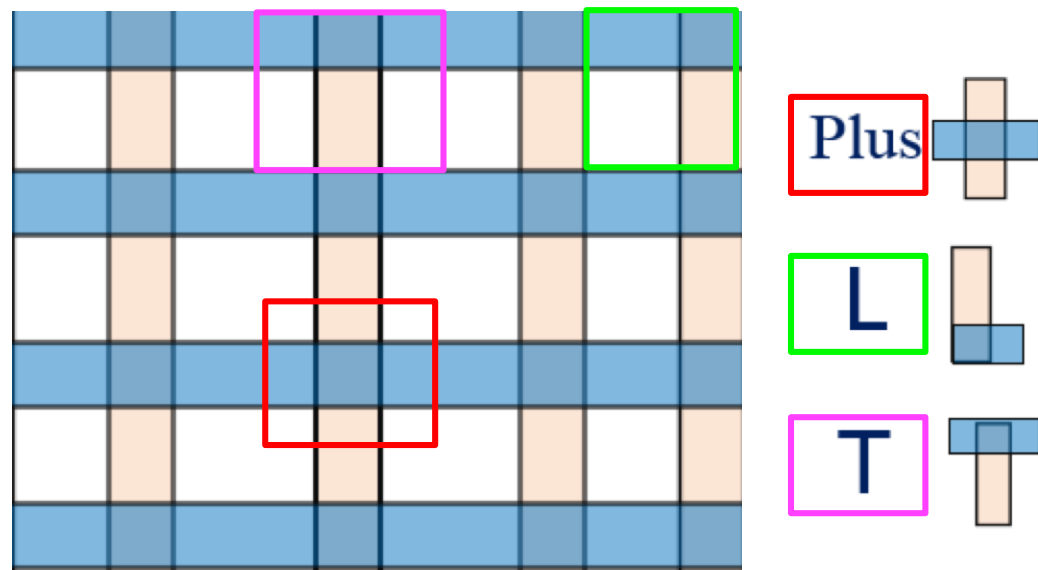
[Mishra, DAC16]

Thermomechanical stress in power grid

- Caused by thermal expansion mismatch between various layers of the interconnect system
- Evaluate using Finite Element Method (**FEM**)
- FEM: Numerical, **computationally expensive**



Various layers in typical copper interconnect

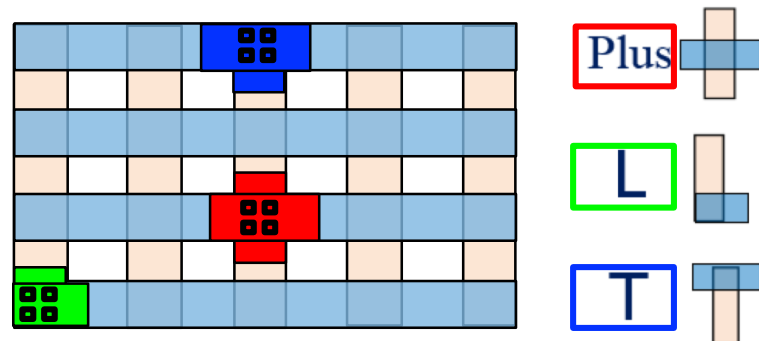


[Mishra, DAC16]

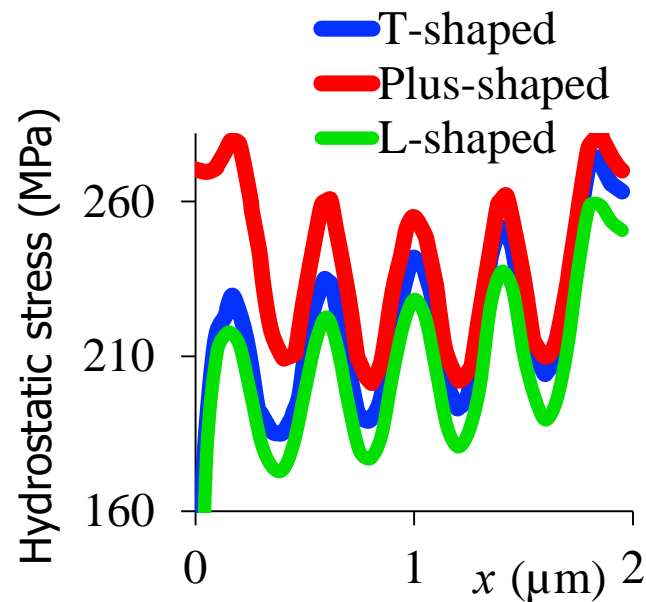
Stress analysis of power grid vias (contd.)

Thermal stress for every via can vary depending on:

- Position of the via array in the power grid
- Position of the via in the via array
- Via array configuration (e.g., 4x4, 8x8 via array)



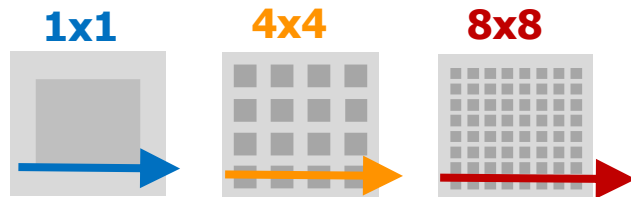
Plus-shaped, T-shaped, and L-shaped 4x4 via array



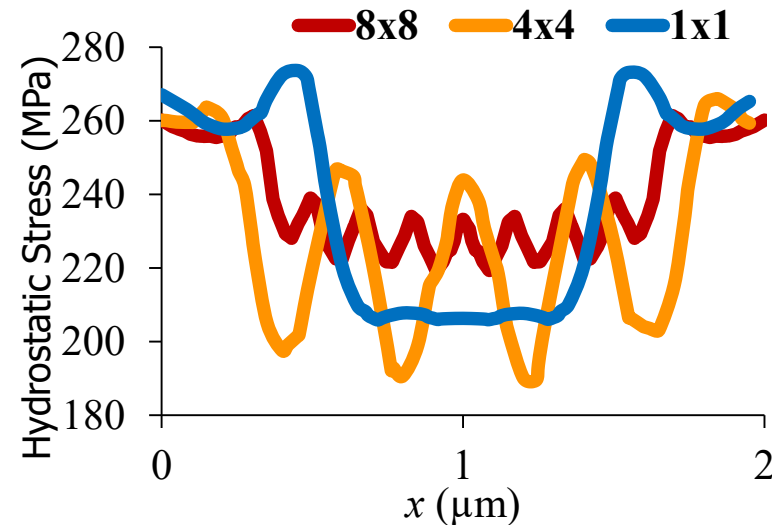
Stress analysis of power grid vias (contd.)

Thermal stress for every via can vary depending on:

- Position of the via array in the power grid
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Three configurations
with the same area

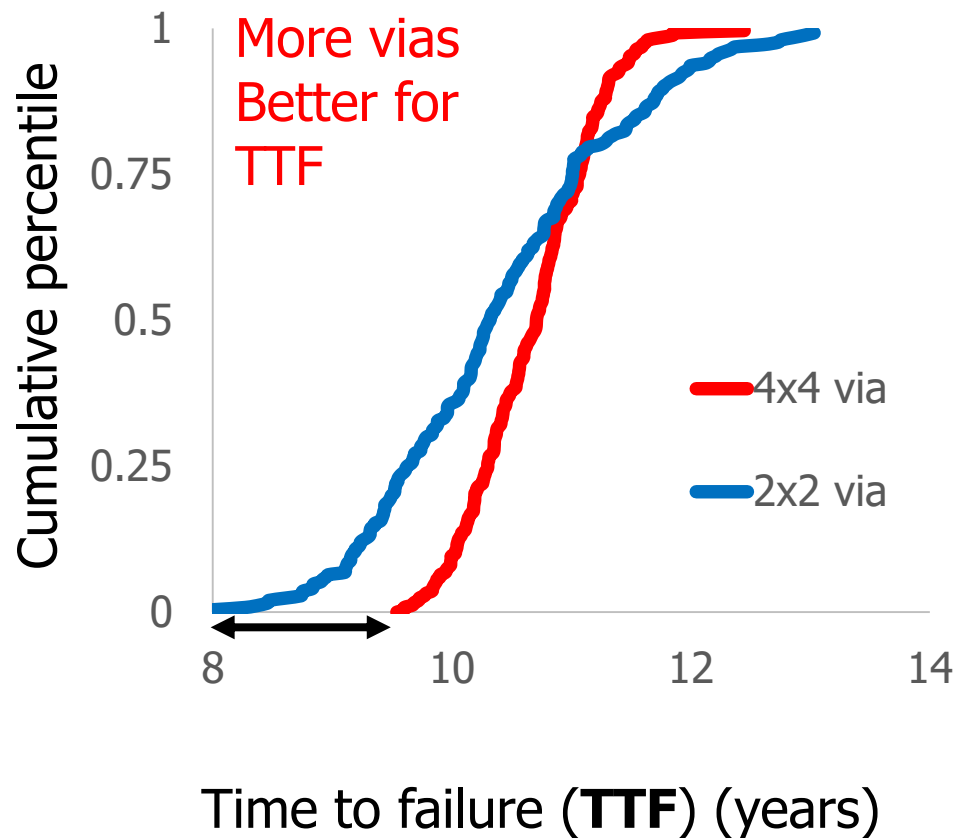
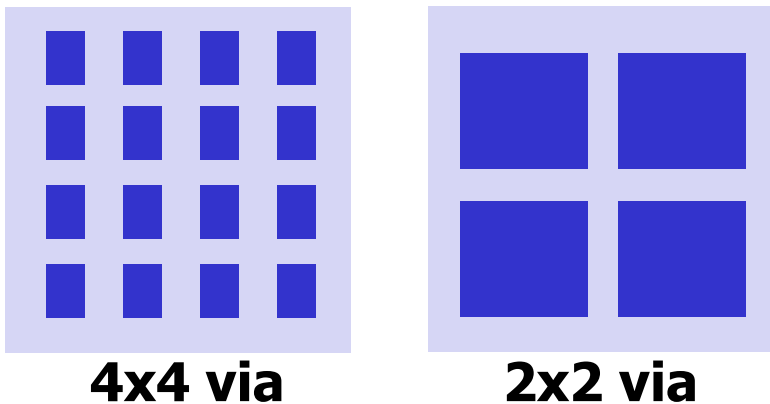


30MPa stress difference = \sim 30% change in lifetime

Via array performance and redundancy

When does the via array fail?

Via arrays with same resistance



[Mishra, DAC16]

IMBPG1: TTF for various failure criteria

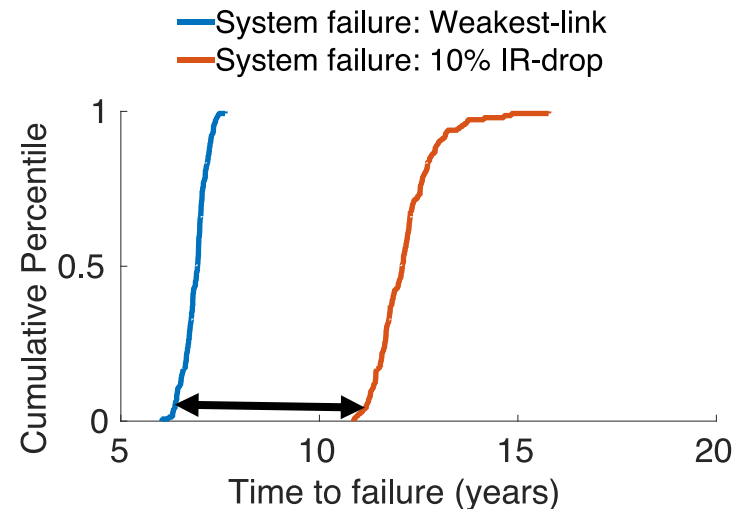
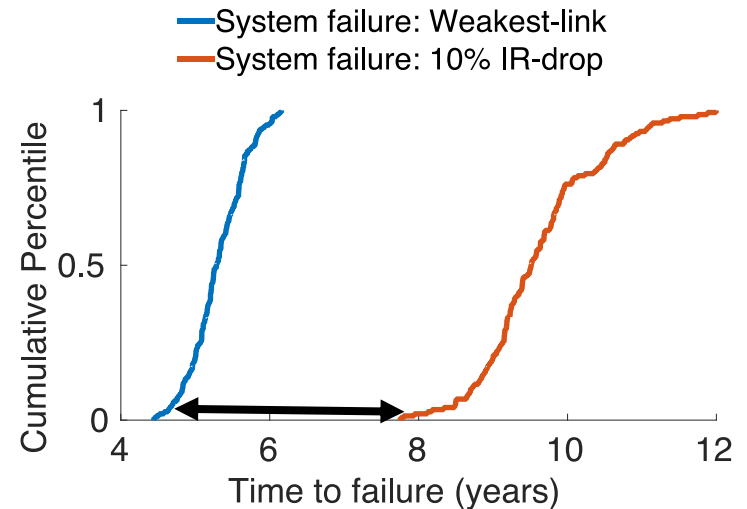
Failure criteria for:

1. System (power grid) failure

- Weakest-link: Conventional method, implies 1st failure
- Our criterion: 10% IR-drop

2. Sub-system (via array) failure

- Weakest-link: 1st via failure
- Our criterion: 8th via failure



[Mishra, DAC16]

Conclusion

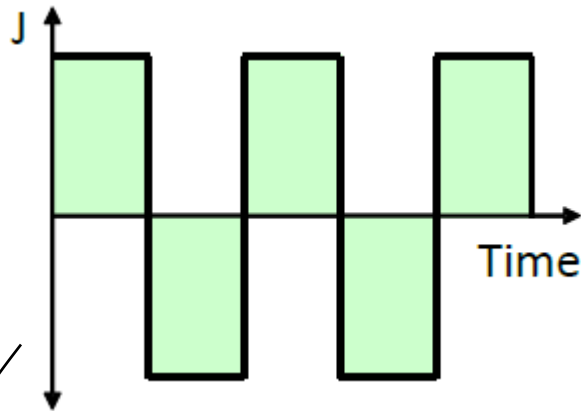
- EM is an important problem for current/future technologies
- Critical issue in high-current density scenarios
 - Lower metal levels
 - Analog blocks
 - Potential within-cell issues
 - Higher on-chip temperatures exacerbate the challenge
- Leveraging redundancy for EM mitigation is essential

Thank you!

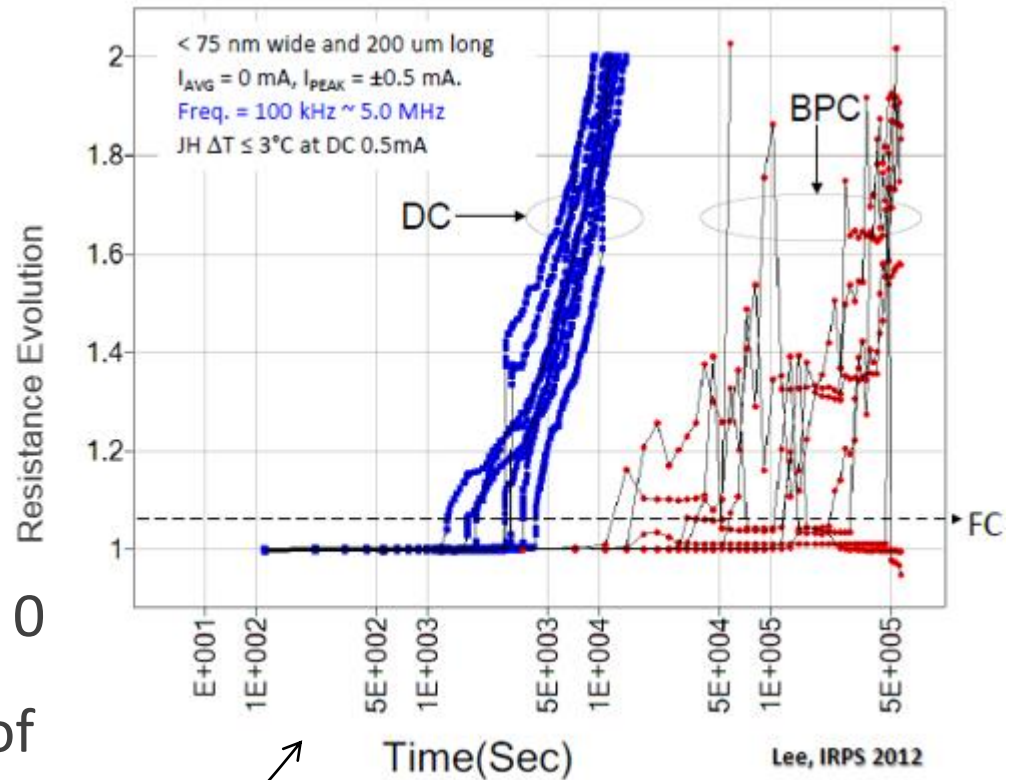
Backup

"AC EM"

Bidirectional pulsed current



- Mathematical average = 0
- Electromigration point of view, failures are seen, but at much higher lifetime
- Define a new 'recovered' current criteria:



$$J = J_{avg}^+ - \mathfrak{R}J_{avg}^-$$